

## **Task**

- The RF Gun reflects power to the klystron. Large amounts of reflected power to the klystron can cause phase and amplitude instabilities in a klystron. Look at pulse shaping as a way to reduce reflected power to the klystron and eliminate the requirement for a 30MW S-Band circulator between the RF Gun and klystron.
- Calculate the reflected power from the RF Gun as a function of the RF input power pulse.
- Increase the power pulse gradually, so the reflected power stays all the time below 4 MW.

## **Method**

- Calculation of the reflected power is carried out in the frequency domain.
- The frequency domain spectrum of the RF input pulse is obtained by the **FFT** on the user defined shape of the input pulse in the time domain.
- Next the Reflection Coefficient  $\Gamma$  is expressed as a function of the cavity Transfer Function near the resonant frequency.
- Reflected signal is calculated as a product of the Fourier transform of RF input signal and the cavity Reflection Coefficient  $\Gamma$ .
- Reflected signal is transformed back into the time domain applying the inverse Fourier Transform, **IFFT**.
- Filling of the cavity – the increase of the cavity electric field is calculated from the input power pulse and parameters of the RF Gun resonator.
- The reflected power and the cavity voltage vs. time are plotted into the same graph.

## Theory

- The general expression for (complex) Reflection Coefficient is:

$$\Gamma = \frac{Z_c - Z_w}{Z_c + Z_w} \quad (1)$$

$Z_c$  is the impedance of the “load”, i.e. the resonant cavity, and  $Z_w$  is the characteristic impedance of the connecting line.

- The impedance of a resonator near its resonant frequency  $\omega_0$  is expressed as:

$$Z_c = \frac{R_{SH}}{1 + j2 \frac{Q_l}{\omega_0} \Delta\omega} \quad (2)$$

$R_{SH}$  is the resonator shunt resistance,  $Q_l$  is the quality factor (including the loading from the external circuits) and detuning  $\Delta\omega = \omega - \omega_0$ ,  $\Delta\omega \ll \omega_0$ . Here  $\omega$  is the frequency independent variable and  $\omega_0$  is the resonant frequency.

- The cavity coupling coefficient  $\beta$  is defined as  $\beta = R_{SH}/Z_w$ .

Substituting for  $R_{SH}$  in (2) and combining (1) and (2), the expression for the Reflection Coefficient in terms of resonator parameters is given

$$\Gamma(\Delta\omega) = \frac{\beta - 1 - j2\tau\Delta\omega}{\beta + 1 + j2\tau\Delta\omega} \quad (3)$$

$\tau$  is cavity filling time constant,  $\tau = Q_l/\omega_0$ .

- The frequency spectrum of the input signal into the cavity is calculated from the shape of the input power pulse as  $V(\Delta\omega) = \text{FFT}\{\sqrt{p(t)}\}$ .
- The reflected signal in the frequency domain can be directly calculated as  $V_{\text{refl}}(\Delta\omega) = V(\Delta\omega)\Gamma(\Delta\omega)$ . (4)

- The Inverse Fast Fourier Transform, (IFFT), transforms this result back into the time domain,

$$v(t) = \text{IFFT}\{V_{\text{refl}}(\Delta\omega)\} \quad (5)$$

- The reflected power is plotted as a function of time using the square of the  $v(t)$ .

- The exponential increase of cavity electric field is calculated from the input power pulse, cavity shunt impedance  $R_{SH}$  and the cavity time constant  $\tau$ . It rises as  $(1 - e^{-t/(2\tau)})$ .

### **Program/Calculation**

- The MATLAB program is used to calculate reflected power and to plot the results.
- User can define the shape of the input power pulse and the other relevant parameters of the RF gun resonator
  - coupling coefficient  $\beta$  (= 2.1),
  - cavity (unloaded) quality factor  $Q_0$  (=13369),
  - cavity shunt impedance  $R_{SH}$  (=1.65 M $\Omega$ ).
- The input and reflected power is expressed in MW, the developed cavity voltage signal in MV.
- Program is available and can be tested and used by anyone interested.

### **Results**

- Present MATLAB plots – the results are calculated for the parameters given above.
- The input power pulse has 4 intermediate steps, the height of each step is 25% of the maximum power. The duration, (width), of those steps is 4x, 5x, 5x, 4x of a single interval of the control clock step, 8.4 ns.

### **References**

- 1) Zenghai Li: Reflection Isolator using a Hybrid and a Dummy Cavity for the LCLS RF Gun., SLAC/LCLC, (2005)
- 2) Jens Knobloch: Basic Concepts of Measurements Made on Superconducting RF Cavities., SRF note, #910927-07, (1991)
- 3) Tom Hays: Cavity Analysis By Reflection, SRF note # 940525-04, (1994)

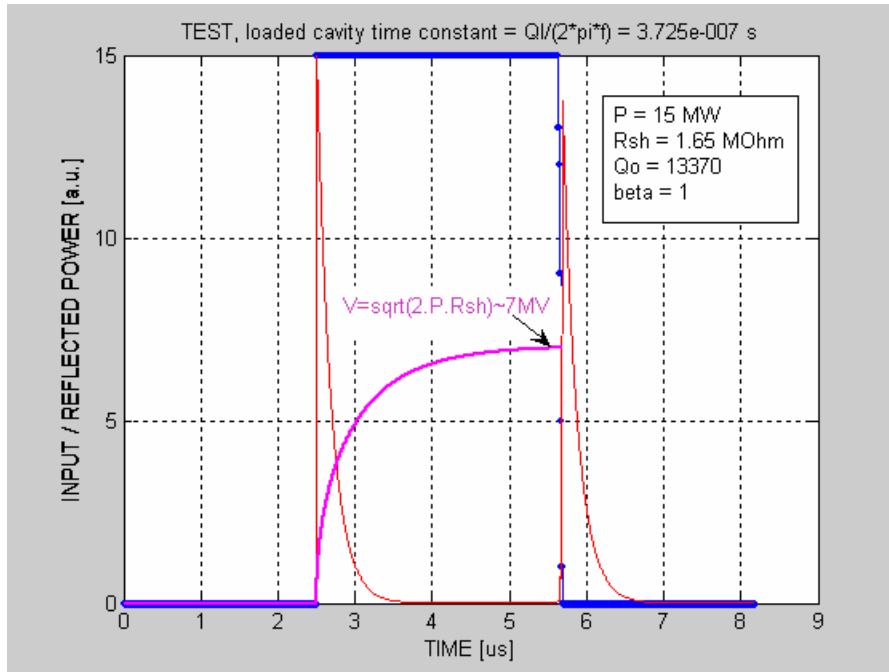


Fig. 1 Test of the program, for given cavity parameters and  $\beta = 1$ .

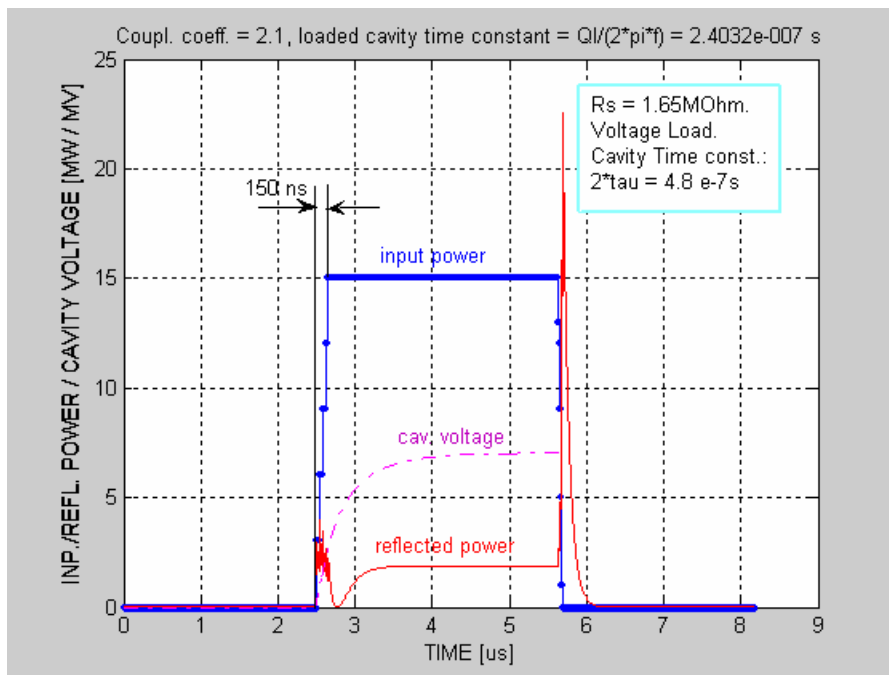


Fig. 2 Five-step shape of the input power pulse keeps reflected power below 4 MW.

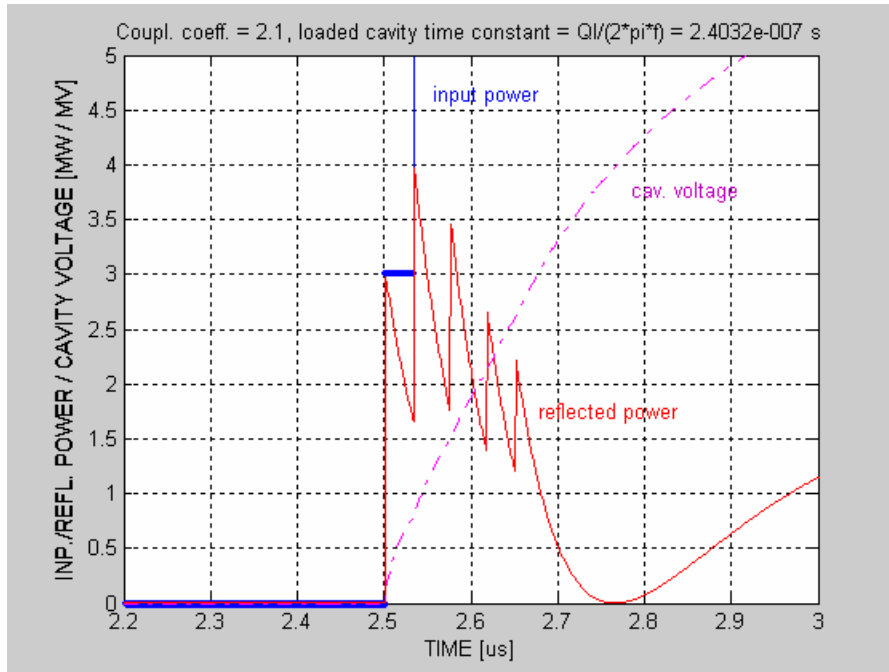


Fig. 3. Detail of reflected power.

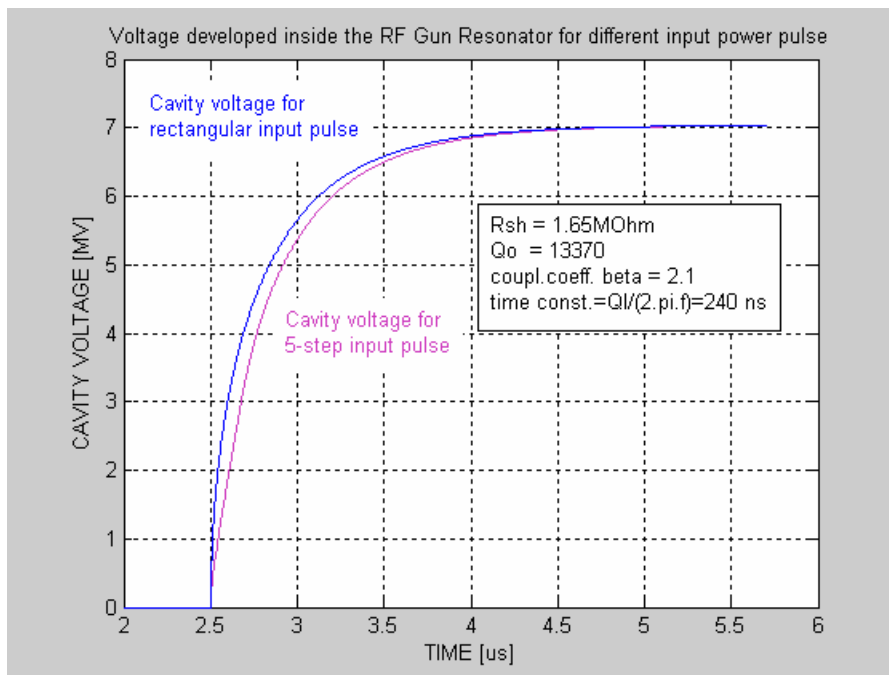


Fig. 4. Rise of the cavity electric field, (voltage), for the input step function and 5-step pulse.

Input power pulse with a linear ramp increase

